

# Desensitization of optical systems Paul Fuller

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### Methods to ensure that a final optical design not only meets its optical specification, but is easily manufacturable.

- Design inputs
- Compensation verses tight tolerances
- Determining sensitivity of tolerances
- Tolerancing methods
- Desensitization by opto-mechanical design choice
- Desensitization by analysis (MTF, aberrations...)
- Desensitization by optimization
- Conclusion/ Further prospects



- System specification
- Choose the 'type' of optical design for the problem
  - Use of proven data bases
  - Use of complex surface types (aspheric, diffractive, free form....)?
- Cost target for the system
  - Price acceptable for individual lenses and mechanical parts
  - Integration time
- Industrial constraints
  - General manufacturing tolerances / capabilities
  - Special manufacturing technologies available
  - Supply chain accessibility and Make/Buy scenario



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**Early in the design phase, the following CodeV® functions enable us to determine the most senstive tolerances / surfaces in the system** 

- Third Order aberration analysis (THO SA ; GO)
  - This enables us to determine the surfaces with the largest aberration transfer, which are likely to be the most sensitive (rough estimate).
- Optimization analysis (AUT ; SNS Sk ; WTC 0 ; go)
  - Running the SNS option in AUT for each surface can highlight surfaces which are sensitive to tilt tolerances.
- Wavefront Differential tolerancing (TOR)
  - This is the most complete 'rapid' method to evaluate the sensitivity of the the different tolerances but can be inaccurate (MTF drops are approximations).
  - Requires the user to create a full set of tolerances and to set up the TOR function
  - Either:
    - (SNS) The same tolerance value is assigned to each surface and the TOR is run to establish where the largest losses occur. OR
    - (INV) A loss of X points of MTF (typically 1 or 2) the value for each tolerance is calculated

#### We are not interested in the final MTF value at this point!!

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#### Relationships between aberrations and sensitivity

- The more powerful an optical surface and the larger the pupil on this surface => the more sensitive the optical surface is likely to be to manufacturing errors.
- The larger the aberration produced (or compensated) by a surface, the more sensitive it is likely to be.
- Use third order aberration analysis 'THO SA' to establish early in the design phase where the large aberration transfers occur.



	SA	TCO	TAS	SAS	PTB	DST	AX	LAT	PTZ
1	-0.578171	-0.743585	-1.332084	-1.119567	-1.013309	-0.479958	-0.344887	-0.147853	-0.012322
2	-0.303926	2.145623	-4.941633	-1.575534	0.107516	3.707596	-0.179436	0.422254	0.001307
3	0.807140	-3.821298	6.339923	2.319605	0.309445	-3.660621	0.391991	-0.618610	0.003763
4	0.507304	1.889186	3.462894	1.899499	1.117802	2.357894	0.400703	0.497402	0.013593
STO	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
6	-0.004343	-0.103773	-0.867542	-0.316471	-0.040935	-2.520870	-0.042743	-0.340476	-0.000498
7	-0.126395	-0.540875	-0.894330	-0.379989	-0.122818	-0.542021	-0.018079	-0.025788	-0.001494
8	-0.410482	1.226398	-1.793949	-0.979703	-0.572579	0.975686	-0.219828	0.218927	-0.006963

 For this Tessar lens, the airgap between L1 and L2 has a large transfer of aberrations and is likely to be sensitive.



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#### Iterations using 'TOR' to find a good set of compensators:

CV code	Compensator type	Lens N°	Effect
CMP DSZ S12	Axial	L1	
CMP DSZ S34	Axial	L2	
CMP DSZ S68	Axial	D3/4	
CMP DIS S12	Radial	L1	
CMP DIS S34	Radial	L2	
CMP DIS S68	Radial	D3/4	
CMP DLZ Si	Axial	Image	

• Axial position and centering of L1 controls the airgap L1 -> L2

- Centering of D3/4 controls the dissymetrie in the system from the remaining tolerances
- Back focus recovers the remaining focus errors
- We are not surprised to find that the airgap between L1 and L2 needs to be controlled as we have already seen the results from the 3<sup>rd</sup> order aberration analysis



## Mechanical design choice



- Zooming of sensitive parameters (with pertubated configurations)
- Minimize angle of incidence on critical surfaces (AOI Sk < X°)</li>
- Control and limit surface curvature, lens power and air gap power
- Careful use of weightings within the optimisation
- Ray targeting for specific aberration control



• MTF optimization –close to the finished, this can be used to balance the TFMTF curves (through focus MTF).

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- Tilt Sensitivity (SNS) (SNS Sk;WTC X)
  - Used in 'aut' optimization to desensitize surfaces to tilt errors. Sensitivity to surface tilt can be linked to other manufacturing errors (lens tilt, lens decenters etc...)
  - Linked to Coma (and almost to Lateral Color), proportional to the output of THO SA;GO



#### • Sensitivity As Built (SAB)

- The SAB optimization routine should be used in a similar way to the MTF optimization routine. Once a locally optimized solution is found, SAB is used to increase 'as-built' performance at the cost of nominal performance
- SAB option allows for compensators inputs.
- Only the most critical tolerances should be included in the optimization to minimize calculation time.
- The calculation is similar (or the same?) as the TOR Wavefront Differential calculation
- Needs to be set up correctly to ensure good results



- Importance to take into account the sensitivities at the earliest stages of the design.
- Knowledge of simple 'rule of thumb' methods for finding the most sensitive parts of a design
- Knowledge of the 'smart' options (SAB, SNS...) with their limitations is necessary.
- Although helpful (time savings), tools never replace the need of experience in optical design.